

The Nonequilibrium Distribution function

- If a distribution changes with time, then it is a non-equilibrium distribution.
- Consider the following:
 - Gas confined to the center of a large container.
 - The confining walls are removed.
 - The gas expands to fill the container.
 - The gas reaches equilibrium with the new volume.
 - What are the properties of the distribution before equilibrium is reached?
 - What role do collisions play in the evolution of the nonequilibrium distribution?
- Like the equilibrium distribution, the nonequilibrium distribution depends on:
 - velocity
 - position
- In addition the distribution depends on time.

- Thus the nonequilibrium distribution function, f^* may be written as:

$$f^*(v_x, v_y, v_z, x, y, z, t) dv_x dv_y dv_z dx dy dz$$

which may be interpreted that a molecule at time t is in the volume $dx dy dz$ located at (x, y, z) with velocity in the range $dv_x dv_y dv_z$ at (v_x, v_y, v_z) .

- Note that the nonequilibrium distribution function, f^* , depends explicitly on t as well as through the coordinates (x, y, z) and velocities (v_x, v_y, v_z) .
- The derivative of f^* with respect to time is:

$$\begin{aligned} \frac{df^*}{dt} = & \frac{\partial f^*}{\partial v_x} \frac{dv_x}{dt} + \frac{\partial f^*}{\partial v_y} \frac{dv_y}{dt} + \frac{\partial f^*}{\partial v_z} \frac{dv_z}{dt} \\ & + \frac{\partial f^*}{\partial x} \frac{dx}{dt} + \frac{\partial f^*}{\partial y} \frac{dy}{dt} + \frac{\partial f^*}{\partial z} \frac{dz}{dt} + \frac{\partial f^*}{\partial t} \end{aligned}$$

- Consider the three terms involving the coordinates:

$$\frac{\partial f^*}{\partial x} \frac{dx}{dt} + \frac{\partial f^*}{\partial y} \frac{dy}{dt} + \frac{\partial f^*}{\partial z} \frac{dz}{dt}$$

- Note that $dx/dt = v_x$, $dy/dt = v_y$, and $dz/dt = v_z$
- Note that $\partial f^*/\partial x$, $\partial f^*/\partial y$, and $\partial f^*/\partial z$ are the spatial gradients of f^* .
- This can be written in vector short hand notation:

$$\frac{\partial f^*}{\partial x} \frac{dx}{dt} + \frac{\partial f^*}{\partial y} \frac{dy}{dt} + \frac{\partial f^*}{\partial z} \frac{dz}{dt} = \nabla f^* \cdot \mathbf{v}$$

where $\nabla = \partial/\partial x + \partial/\partial y + \partial/\partial z$, \mathbf{v} is the velocity vector and \cdot means the vector dot product. (∇ may be read as “nabla” or “grad”.)

- Now consider:

$$\frac{\partial f^*}{\partial v_x} \frac{dv_x}{dt} + \frac{\partial f^*}{\partial v_y} \frac{dv_y}{dt} + \frac{\partial f^*}{\partial v_z} \frac{dv_z}{dt}$$

- Note that dv_x/dt , dv_y/dt , and dv_z/dt are the components of acceleration vector \mathbf{a} and that $\mathbf{F}_{\text{ext}} = m\mathbf{a}$. Therefore:

$$\frac{\partial f^*}{\partial v_x} \frac{dv_x}{dt} + \frac{\partial f^*}{\partial v_y} \frac{dv_y}{dt} + \frac{\partial f^*}{\partial v_z} \frac{dv_z}{dt} = \nabla_v f^* \cdot \frac{\mathbf{F}_{\text{ext}}}{m}$$

- Therefore:

$$\frac{df^*}{dt} = \nabla f^* \cdot \mathbf{v} + \nabla_v f^* \cdot \frac{\mathbf{F}_{\text{ext}}}{m} + \frac{\partial f^*}{\partial t}$$

- When

$$\frac{\partial f^*}{\partial t} = 0$$

the system is in a steady state or at equilibrium.

- In a steady state, the properties of the system at a particular point in space do not change with time.

- When

$$\nabla_v f^* \cdot \frac{\mathbf{F}_{\text{ext}}}{m} = 0$$

There are no external forces on the system.

- When something is being transported

$$\nabla f^* \cdot \mathbf{v} \neq 0$$

The Molecular Basis of f^*

- Recall that f^* is proportional to a probability.
 - We are concerned with molecular concentrations or number density.
- If the system is not at equilibrium, then we are concerned with number densities that depend on position and N/V is an insufficient description.

$$\begin{aligned}
dN &= n(x, y, z, t)(f^*(v_x, v_y, v_z, x, y, z, t)d^3\mathbf{v}d^3\mathbf{r}) \\
&= F^*(v_x, v_y, v_z, x, y, z, t)d^3\mathbf{v}d^3\mathbf{r}
\end{aligned}$$

where

- dN is the number of molecules at time t in the six-dimensional volume element defined by the velocity and position coordinates $d^3\mathbf{v}d^3\mathbf{r} = dv_x dv_y dv_z dx dy dz$.
- F^* is the number density distribution function, $F^* = n f^*$.
- Consider the evolution of the number density distribution function through the time interval dt .
 - Molecules move due to their velocity and any acceleration caused by external forces.
 - Positions change from \mathbf{r} to $\mathbf{r}' = \mathbf{r} + \mathbf{v} dt$
 - Velocities change from \mathbf{v} to $\mathbf{v}' = \mathbf{v} + \mathbf{a} dt$
 - The number, dN' , in $d^3\mathbf{v} d^3\mathbf{r}$ at \mathbf{r}' and \mathbf{v}' is:

$$dN' = F^*(\mathbf{v}', \mathbf{r}', t + dt)d^3\mathbf{v} d^3\mathbf{r}$$

- But collisions may cause molecules to enter or leave the volume element $d^3\mathbf{v} d^3\mathbf{r}$. The contribution this makes is dN_{coll}

$$dN' - dN = dN_{coll}$$

Therefore

$$dN_{coll} = [F^*(\mathbf{v}', \mathbf{r}', t + dt) - F^*(\mathbf{v}, \mathbf{r}, t)] d^3\mathbf{v} d^3\mathbf{r}$$

But

$$[F^*(\mathbf{v}', \mathbf{r}', t + dt) - F^*(\mathbf{v}, \mathbf{r}, t)] = dF^* = \frac{dF^*}{dt} dt$$

Therefore

$$dN_{coll} = \frac{dF^*}{dt} dt d^3\mathbf{v} d^3\mathbf{r}$$

Analogous to the treatment of f^* :

$$\frac{dF^*}{dt} = \nabla F^* \cdot \mathbf{v} + \nabla_v F^* \cdot \frac{\mathbf{F}_{\text{ext}}}{m} + \frac{\partial F^*}{\partial t}$$

and

$$dN_{coll} = \left(\nabla F^* \cdot \mathbf{v} + \nabla_v F^* \cdot \frac{\mathbf{F}_{\text{ext}}}{m} + \frac{\partial F^*}{\partial t} \right) dt d^3\mathbf{v} d^3\mathbf{r}$$

- Now collisions must be considered explicitly.
 - dN_{coll} is the net change of molecules scattered in and out of $d^3\mathbf{v} d^3\mathbf{r}$ in time dt .
 - The rate of change of this with time is:

$$\frac{dN_{coll}}{dt} = (\text{time rate of change of } F^*) d^3\mathbf{v} d^3\mathbf{r}$$

- Finding the time rate of change is difficult. The result is the *Boltzmann Transport Equation* which is difficult to solve.
 - Need to use approximations instead.
- Consider a system sufficiently close to equilibrium that $F^* \cong F$.
 - F is the equilibrium number density distribution function Nf/V .
 - If the system is isolated, F^* should go smoothly and quickly toward F .
- Consider Ar(g) at equilibrium at 300 K.
 - Alter the equilibrium by taking half the molecules at $v_x=250 \text{ m s}^{-1}$ and reverse their direction.

- The distribution will be the equilibrium distribution except for spikes at $v_x = \pm 250 \text{ m s}^{-1}$.
- The system then *relaxes* smoothly toward equilibrium.
- Consider first the spike at $v_x = -250 \text{ m s}^{-1}$.
 - $f^* > f$ or $f^* - f > 0$. Therefore $df^*/dt < 0$.
 - The spike drops until equilibrium is reached.
- For the spike at $v_x = +250 \text{ m s}^{-1}$.
 - $f^* < f$ or $f^* - f < 0$. Therefore $df^*/dt > 0$.
 - The spike rises until equilibrium is reached.
- Thus it can be shown that df^*/dt , dF^*/dt , and dN_{coll}/dt have the same sign and that the sign is opposite to that of $(f^* - f)$ or $(F^* - F)$.
- When F^* is not far from F it may be assumed that dN_{coll}/dt is directly proportional to the difference between F^* and F

$$(\text{time rate of change of } F^*) \propto (F^* - F)$$

- This is known as the *linear response regime*.

- What affects the proportionality factor?
- Since it is collisions that cause the relaxation, the average time between collisions τ_{coll} will be involved. If it is assumed that this is the proportionality factor, then:

$$\frac{dN_{coll}}{dt} = \frac{F^* - F}{\tau_{coll}} d^3\mathbf{v} d^3\mathbf{r}$$

- Thus, in the linear response regime, the Boltzmann transport equation become linearized:

$$\nabla F^* \cdot \mathbf{v} + \nabla_v F^* \cdot \frac{\mathbf{F}_{ext}}{m} + \frac{\partial F^*}{\partial t} = - \frac{F^* - F}{\tau_{coll}}$$

What is τ_{coll} ?

- Consider λ , the mean free path or the average distance travelled between collisions.
- Consider the cross section σ
 - A cross section may be determined for **any** type of interaction potential.
 - For most potentials, the cross section varies with relative speed of the collision partners.

- Collision cross sections for slow speeds can be larger than those for faster speeds since the molecules have more time to interact under the influence of the interaction potential.
- A velocity-specific free path needs to be considered.

$$\lambda(\mathbf{v}) = v\tau_{coll}(\mathbf{v})$$

where:

- $\lambda(\mathbf{v})$ is the free path of a molecule with velocity \mathbf{v} ,
- v is the speed corresponding to velocity \mathbf{v} ,
- $\tau_{coll}(\mathbf{v})$ is the time between collisions for a molecule with velocity \mathbf{v} .
- $v\tau_{coll}(\mathbf{v})$ is the distance travelled at speed v before the next collision.
- We must now get the average of $\tau_{coll}(\mathbf{v})$ over all velocities.
- The collision rate is the reciprocal of τ_{coll} , i.e. τ_{coll}^{-1}

- To determine the collision rate:
 - Consider molecules with velocity \mathbf{v}_1 colliding with molecules of velocity \mathbf{v} .
 - The relative speed of these molecules is $g = |\mathbf{v}_1 - \mathbf{v}|$
 - The collision cross section is $\sigma(g)$
 - n is the number density of target molecules with velocity \mathbf{v} .
 - The flux of molecules with velocity \mathbf{v}_1 toward the collision partners is gn .
- The collision rate for molecules with velocity \mathbf{v}_1 is the product of flux and cross section.

$$\tau_{coll}^{-1}(\mathbf{v}_1) = gn\sigma(g)$$

- Consider (see Figure 25.2) a frame of reference in which the target molecules are still (i.e. both the frame of reference and the target molecules are moving with velocity \mathbf{v}).
- The unit area holding the target molecules is considered as the end of a solid of length $g dt$.
 - The target molecules take up a fraction of this unit area.

- The solid defines a volume containing a flux of molecules that are moving with uniform speed g
- In the time, dt , all the molecules contained in the volume moving with speed g will move through the unit area unless they collide with a target molecule.
- We can find the average collision rate for one molecule of type 1:

$$z_1 = \tau_{coll}^{-1} = \int g \sigma(g) F^*(\mathbf{v}) d^3\mathbf{v} = n \langle g\sigma \rangle$$

- If a system is at equilibrium, this is a constant.
- If a system is not at equilibrium, then n depends on time and space.
- Recall that:

$$\lambda(\mathbf{v}) = v\tau_{coll}(\mathbf{v})$$

- Thus at conditions of equilibrium:

$$\lambda = \int \lambda(\mathbf{v}) f(\mathbf{v}) d^3\mathbf{v} = \frac{\langle v \rangle}{n \langle g\sigma \rangle}$$

- If σ is independent of velocity then $\langle g\sigma \rangle = \langle g \rangle \sigma$ and $\langle g \rangle = \sqrt{2}\langle v \rangle$
- At equilibrium $n = N/V$, therefore:

$$\lambda = \frac{\langle v \rangle V}{N\sqrt{2}\langle v \rangle \sigma} = \frac{V}{\sqrt{2}N\sigma}$$

(which is the equation we previously derived).

- The mean collision rate gives an upper limit on reaction rates.
 - Why don't all collisions lead to reaction?

Collisions between Unlike Molecules

- The cross section for a collision depends specifically on the types of molecules undergoing collision.
- Consider a binary mixture of gases 1 and 2.
 - σ_{11} is the cross section for collision of a type 1 molecule with another molecule of type 1.
 - σ_{22} is the cross section for collision of a type 2 molecule with another molecule of type 2.
 - σ_{12} is the cross section for collision of a type 1 molecule with another molecule of type 2.

- With hard sphere molecular diameters of d_1 and d_2 , the cross sections are:

$$\sigma_{11} = \pi d_1^2$$

$$\sigma_{22} = \pi d_2^2$$

$$\sigma_{12} = \frac{\pi(d_1 + d_2)^2}{4}$$

- The mean collision rate for molecules of type 1 with molecules of type 2.

$$z_{12} = n_2 \langle g \rangle \sigma_{12} = n_2 \left(\frac{8k_B T}{\pi \mu_{12}} \right)^{1/2} \sigma_{12}$$

where μ_{12} is the reduced mass of molecule 1 with molecule 2.

- Note the dependence of this rate on the number density of molecule 2, the target molecule.

Total Collision Rate per Unit Volume

- The total collision rate per unit volume is the collision rate per molecule times the number density for that molecule.

- If there is one component in the gas:

$$Z_{11} = \frac{1}{2}nz_1 = \frac{1}{2}\langle g\sigma \rangle n^2 = \frac{\sigma \langle v \rangle}{\sqrt{2}}n^2$$

where the factor of 1/2 ensures that collisions are not double counted.

- If there are two components in the gas, then:

$$Z_{12} = n_1z_{12} = n_2z_{21} = \langle g\sigma \rangle n_1n_2$$

where $\langle g\sigma \rangle \cong \langle g \rangle \sigma_{12}$

- See the summary in table 25.1

Macroscopic Non-equilibrium Phenomena

- We will consider
 - Diffusion
 - Thermal conduction
 - Electrical conduction
 - Viscosity
- The evolution of nonequilibrium systems is governed by the Second Law of Thermodynamics.
 - In an isolated system, a spontaneous process will continue until maximum entropy is reached subject to the constraints of the system.

- Nonequilibrium thermodynamics may be considered in terms of the time dependence of entropy.
- Recall the formulation of chemical potential (μ) in terms of the minimization of the potential and the maximization of entropy.
 - Chemical potential gradients will drive the system toward equilibrium.
 - These gradients are of macroscopic parameters such as temperature, concentration, or density.
- For a system at equilibrium:

$$\mu(T, P) = \mu^\circ(T) + RT \ln \left(\frac{P}{1 \text{ bar}} \right)$$

- Consider a closed system with a temperature gradient in the x direction and with uniform pressure.
 - The chemical potential gradient is:

$$\frac{\partial \mu}{\partial x} = \frac{\partial \mu}{\partial T} \frac{\partial T}{\partial x} = \frac{\partial(\mu^\circ + RT \ln P)}{\partial T} \frac{\partial T}{\partial x}$$
 - The spatial derivative of thermodynamic potential (in this case $\partial T / \partial x$) act as the forces that drive transport phenomena.

- The mathematical formulation of diffusion, thermal conduction, electrical conduction, and viscosity are all similar.
- Recall the wall collision rate, J_x , or flux of molecules moving through a plane in the gas.
 - All transport phenomena may be treated in terms of the vector flux of a transported quantity.

$$\text{Flux} = \mathbf{J}(\text{something})$$

$$= \frac{\text{amount of something moving in given direction}}{(\text{unit area})(\text{unit time})}$$

- This may be applied to:
 - diffusion - transport of matter
 - thermal conduction - transport of energy
 - electrical conduction - transport of charge
 - viscosity - transport of linear momentum
- Flux increases, the further a system is from equilibrium.
 - Distance from equilibrium may be measured by the magnitude of simple gradients of macroscopic parameters.

$$\mathbf{J}(\text{something}) = -(\text{phenomenological coefficient}) \\ \times (\text{gradient of a macroscopic parameter})$$

Diffusion

- Consider the diffusion of matter, where z is the direction of the flux of matter.

$$J_z = -D \left(\frac{\partial n}{\partial z} \right)$$

where:

- D is the diffusion coefficient
- $(\partial n / \partial z)$ is the density gradient.
- The negative sign indicates that the flux is in the direction opposite that of the gradient.
- This equation is known as Fick's first law.
- This equation applies if the system is not far from equilibrium (i.e. in the linear response regime.)

- If the system is far from equilibrium, then the situation is more complex.
- Consider binary diffusion:
 - For example a drop of dye in water. The dye diffuses through the water until the composition is uniform.
 - Binary diffusion is defined in terms of two distinguishable species moving through each other.
- Self diffusion involves only one species.
 - May be monitored experimentally by isotopic labelling.
 - May be monitored by optical properties such as light scattering.
 - May be monitored by nuclear spin properties (NMR).
- Consider a density gradient in the z direction:
 - The flux into a region from z to $z + dz$ is given by Fick's first law evaluated at z :

$$J_{n,z} = -D \left(\frac{\partial n(z)}{\partial z} \right)$$

- The flux out of this region is given by Fick's first law evaluated at $z + dz$:

$$J_{n,z+dz} = -D \left(\frac{\partial n(z + dz)}{\partial z} \right)$$

$$= -D \left[\left(\frac{\partial n(z)}{\partial z} \right) + \left(\frac{\partial^2 n(z)}{\partial z^2} \right) dz \right]$$

where:

$$n(z + dz) = n(z) + dn(z) = n(z) + \left(\frac{\partial n(z)}{\partial z} \right) dz$$

- The difference between flux in and flux out, per unit distance, is:

$$\frac{J_{n,z} - J_{n,z+dz}}{dz} = \frac{\partial n(z)}{\partial t}$$

- Substitution for $J_{n,z}$ and $J_{n,z+dz}$ gives:

$$\frac{\partial n(z, t)}{\partial t} = D \left(\frac{\partial^2 n(z, t)}{\partial z^2} \right)$$

which is Fick's second law.

- Fick's second law accounts for nonlinear concentration gradients.
 - If a gradient were perfectly linear and stable in time, then

$$\left(\frac{\partial^2 n(z, t)}{\partial z^2} \right) = 0; \left(\frac{\partial n}{\partial t} \right) = 0$$
 - Spontaneous fluctuations characterized by large values of $(\partial^2 n(z, t)/\partial z^2)$ which change rapidly with time.
- Solutions to Fick's second law depend strongly on the initial conditions.

An Example of Diffusion

- Initially the solute is contained in a yz plane at $x = 0$ and $t = 0$.
- Let it diffuse from $x = 0$ to $x = \pm\infty$
- Experimentally this may be achieved by coating a thin plate on both sides with the solute and inserting it into the solvent.
- The solution to Fick's second law is:

$$n(x, t) = \frac{N_0}{A\sqrt{4\pi Dt}} e^{-x^2/4Dt}$$

- Conservation of the number of molecules gives the normalization condition:

$$\int_{-\infty}^{\infty} n(x, t) dx = \frac{N_0}{A}$$

- Note also that this solution of Fick's second law is in the form of the Gaussian function, i.e.:

$$\exp \left[- \left(\frac{\text{distance}}{\text{width}} \right)^2 \right]$$

- In this case width = $(4Dt)^{1/2}$.
- Note the dependence on the square root of time.
- As the concentration gradients lessen, diffusion slows down.
- The solution to Fick's second law may be thought of in terms of a time dependent distribution function with the fraction of molecules at a particular time and position given by:

$$f(x, t) = \frac{1}{\sqrt{4\pi Dt}} e^{-x^2/4Dt}$$

- The rms spread in x may be determined:

$$\begin{aligned}
 x_{rms} &= \left[\int_{-\infty}^{\infty} \frac{x^2}{\sqrt{4\pi Dt}} e^{-x^2/4Dt} dx \right]^{1/2} \\
 &= \left[\frac{4Dt}{\sqrt{\pi}} \int_{-\infty}^{\infty} y^2 e^{-y^2} dy \right]^{1/2} = (2Dt)^{1/2}
 \end{aligned}$$

Diffusion as a Stochastic Process

- In 1905, Einstein and van Smoluchowski independently explained Brownian motion as a stochastic or random process.
 - Diffusion is one consequence of Brownian motion.
 - Individual molecules collide and as a result the molecules change direction randomly.
 - This may be simulated by a random walk.
- Consider a one dimensional random walk.
 - The initial position is $x = 0$.
 - The particle may move randomly by $x = \pm 1$ each time step.

- What is the probability that the particle has moved X units after N time steps?
- Since there are two choices at each step, there are 2^N possibilities.
- Denote the number of steps in the positive direction as N_+ .
- Denote the number of steps in the negative direction as N_- .
 - The final position is:

$$X = N_+ - N_-$$

- Since the total number of steps taken is $N = N_+ + N_-$,

$$X = N_+ - (N - N_+) = 2N_+ - N$$

or

$$N_+ = \frac{1}{2}(N + X)$$

- The number of ways, W , that N_+ may be achieved are:

$$W = \frac{N!}{N_+!N_-!} = \frac{N!}{N_+!(N - N_+)!}$$

- In terms of position and total number of moves, this becomes:

$$W = \frac{N!}{\left[\frac{1}{2}(N+X)\right]! \left[\frac{1}{2}(N-X)\right]!}$$

- Therefore the probability of arriving X steps from the origin after N steps is:

$$P = \frac{W}{2^N} = \frac{N!}{2^N \left[\frac{1}{2}(N+X)\right]! \left[\frac{1}{2}(N-X)\right]!}$$

- Recall Stirling's Approximation:

$$\ln N! = \left(N + \frac{1}{2}\right) \ln N - N + \ln(2\pi)^{1/2}$$

- Rewriting the probability P in logarithmic form gives:

$$\begin{aligned} \ln P = \ln N! - N \ln 2 - \ln \left\{ \left[\frac{1}{2}(N+X)\right]! \right\} \\ - \ln \left\{ \left[\frac{1}{2}(N-X)\right]! \right\} \end{aligned}$$

Therefore:

$$\begin{aligned}
\ln P = & \left(N + \frac{1}{2}\right) \ln N - N + \ln(2\pi)^{1/2} - N \ln 2 \\
& - \left(\left\{ \left[\frac{1}{2} (N + X) \right] + \frac{1}{2} \right\} \ln \left[\frac{1}{2} (N + X) \right] \right. \\
& \quad \left. - \left[\frac{1}{2} (N + X) \right] + \ln(2\pi)^{1/2} \right) \\
& - \left(\left\{ \left[\frac{1}{2} (N - X) \right] + \frac{1}{2} \right\} \ln \left[\frac{1}{2} (N - X) \right] \right. \\
& \quad \left. - \left[\frac{1}{2} (N - X) \right] + \ln(2\pi)^{1/2} \right)
\end{aligned}$$

Rearranging gives:

$$\begin{aligned}
\ln P = & \left(N + \frac{1}{2}\right) \ln N - \ln(2\pi)^{1/2} \\
& - \left(\left[\frac{1}{2} (N + X + 1) \right] \ln \frac{1}{2} \right. \\
& \quad \left. + \left[\frac{1}{2} (N + X + 1) \right] \ln \left[N \left(1 + \frac{X}{N} \right) \right] \right)
\end{aligned}$$

$$\begin{aligned}
& - \left(\left[\frac{1}{2} (N - X + 1) \right] \ln \frac{1}{2} \right. \\
& \left. + \left[\frac{1}{2} (N - X + 1) \right] \ln \left[N \left(1 - \frac{X}{N} \right) \right] \right)
\end{aligned}$$

Further rearrangement gives:

$$\begin{aligned}
\ln P = & \left(N + \frac{1}{2} \right) \ln N - \ln(2\pi)^{1/2} \\
& - \left[\frac{1}{2} (N + X + 1) \right] \ln \frac{1}{2} - \left[\frac{1}{2} (N - X + 1) \right] \ln \frac{1}{2} \\
& - \left[\frac{1}{2} (N + X + 1) \right] \ln N - \left[\frac{1}{2} (N - X + 1) \right] \ln N \\
& - \left[\frac{1}{2} (N + X + 1) \right] \ln \left(1 + \frac{X}{N} \right) \\
& - \left[\frac{1}{2} (N - X + 1) \right] \ln \left(1 - \frac{X}{N} \right)
\end{aligned}$$

which simplifies to:

$$\begin{aligned}
\ln P = & \ln \left(\frac{2}{\pi N} \right)^{1/2} - \left[\frac{1}{2} (N + X + 1) \right] \ln \left(1 + \frac{X}{N} \right) \\
& - \left[\frac{1}{2} (N - X + 1) \right] \ln \left(1 - \frac{X}{N} \right)
\end{aligned}$$

- This with the the power series for e^x and the fact that X/N is small gives:

$$P = \left(\frac{2}{\pi N} \right)^{1/2} e^{-X^2/2N}$$

which is an unnormalized Gaussian function.

- Normalization (i.e. integration over all space gives 1) yields:

$$\frac{1}{2} \left(\frac{2}{\pi N} \right)^{1/2} e^{-X^2/2N} = \left(\frac{1}{4\pi Dt} \right)^{1/2} e^{-x^2/4Dt}$$

- If it is assumed that a random step covers the distance x_o such that $Xx_o = x$ and the time between steps is τ (i.e. $N = t/\tau$) then:

$$\frac{X^2}{2N} = \frac{x^2\tau}{2x_o^2t} = \frac{x^2}{4Dt}$$

Therefore:

$$D = \frac{x_o^2}{2\tau} = \frac{\lambda^2}{2\tau}$$

- Recall that:

$$\langle \tau_{coll} \rangle = \frac{\lambda}{\langle v \rangle}$$

where $\langle v \rangle$ is the mean speed.

- Therefore:

$$D = \frac{\langle v \rangle \lambda}{2}$$

- Therefore the diffusion is faster the larger the mean free path is.
 - The diffusion coefficient, D , increases as the square of the mean free path.
- Random walks may be studied by computer simulation (Fig. 25.6).
 - The difference between the simulation and theory varies as \sqrt{N} where in this case N is the number of simulations.

Concentration Gradients

- What drives diffusion or any other transport process, are chemical potential gradients.
 - A concentration gradient is just one example of a chemical potential gradient.

- Nonideal systems may have gradients in chemical potential which give rise to concentration gradients.

Diffusion in Solids

- Defects in the crystalline structure are important (See section 16.4 of Winn).
 - Defects can affect how diffusion occurs in a solid.
 - Defect sites themselves can diffuse through the solid.
 - Annealing or tempering is a way to minimize defects in a solid.
- Small molecules such as H_2 or He can diffuse through the interstitial sites in a crystalline solid.
 - Reactions of the solid with the diffusing molecules can change the properties of the solid (i.e. poisoning of a catalyst).
- Consider two pure metals or alloys, A and B

- A and B are a diffusion couple which initially have a distinct interface and diffuse into each other.
- If one metal diffuses into the other much more rapidly, then the Hartley-Kirkendall may be observed.
- Let B be the faster moving metal.
- As diffusion proceeds, the interface of the AB region appears to move towards B.
- Vacancies appear in B as the atoms move into A and diffusion may be interpreted as the movement of the vacancies themselves.
- The mutual diffusion coefficient, D_{AB} is proportional to $x_A D_B + x_B D_A$ where x_A and x_B are mole fractions and D_A and D_B are the self-diffusion coefficients.
- If B diffuses quickly then $D_B \gg D_A$ and as B moves into A, $x_A \gg x_B$.
 - Then $D_{AB} \cong D_B$
- A is moving slowly into B and from that perspective, $D_{AB} \cong D_A$
- The interface moves toward B and as B depletes, vacancies form.

Thermal Conduction

- Encounter it frequently in our day-to-day life.
 - Insulation of walls
 - Heat loss through different types of windows
 - Styrofoam food containers
- Temperature gradient transports energy.

$$J_{q,z} = -k \left(\frac{\partial T}{\partial z} \right)$$

where k is thermal conductivity ($\text{W m}^{-1} \text{K}^{-1}$)

- This equation is known as “Fourier’s Law”.
- What affects the value of k ?
 - For elements, k reflects periodic trends.
 - Metals typically have k between 10-300 $\text{W m}^{-1} \text{K}^{-1}$ (for example Ag has $k= 430 \text{ W m}^{-1} \text{K}^{-1}$) .
 - Diamond has $k= 1370 \text{ W m}^{-1} \text{K}^{-1}$.
 - Graphite has $k= 129 \text{ W m}^{-1} \text{K}^{-1}$.

- Molecular solids have lower k .
 - Red phosphorous $k= 13.2 \text{ W m}^{-1} \text{ K}^{-1}$.
 - White phosphorous $k= 0.44 \text{ W m}^{-1} \text{ K}^{-1}$.
- What affects the ability of solids to conduct heat:
 - The physical state of the system (i.e. polycrystalline or single crystal)
 - Anisotropy of physical structure.
 - Lattice vibrations (phonons), especially insulating materials.
 - Electron mobility in metals and semiconductors (more important than phonons in conducting materials).
- How do liquids conduct heat?
 - Liquids generally have lower conductivity than solids.
 - $k= 0.03 \text{ W m}^{-1} \text{ K}^{-1}$ for liquid He at 4.2 K.
 - $k= 0.10\text{-}0.15 \text{ W m}^{-1} \text{ K}^{-1}$ for most molecular liquids.

- $k = 0.61 \text{ W m}^{-1} \text{ K}^{-1}$ for water.
- $k > 10 \text{ W m}^{-1} \text{ K}^{-1}$ for liquid metals.
- The mechanism for heat transfer is energy transfer in molecular collisions and is related to the speed of sound in the liquid.
 - Therefore thermal conductivity in a liquid is related to heat capacity.
- Thermal conductivity in gases is related to the pressure of the gas.
- Thermal conductivity usually increases with temperature at temperatures above room temperature.
 - The temperature dependence of thermal conductivity in single crystal solids is very nonlinear at low temperature.

Electrical Conduction

- Metals conduct electricity well.
- Insulators do not conduct electricity.
- Semiconductors can conduct electricity, but not as well as metals.

- The high conductivity of metals can be interpreted in terms of the structure of the metals and the mobility of the conduction electrons in the conducting band.
- Ohm's Law is the flux gradient equation for charge transport:

$$J_{e,z} = -\sigma_e \left(\frac{\partial \phi}{\partial z} \right)$$

where:

- $J_{e,z}$ is the electron flux in $\text{C m}^{-2} \text{ s}^{-1}$ or A m^{-2}
- σ_e is the electrical conductivity in S m^{-1} or $\text{A}^2 \text{ s}^3 \text{ kg}^{-1} \text{ m}^{-3}$. (S stands for siemens where $1 \text{ S} = 1 \text{ A V}^{-1}$ and is the reciprocal of the ohm.)
- ϕ is the potential difference in V or J C^{-1}
- z is distance in m.
- A variant of Ohm's Law is $E = IR$ where:
 - E is the electromotive force or voltage.
 - I is the current

- R is the resistance (which is the reciprocal of the conductance.)
- The relationship between resistance and conductivity is:

$$\sigma_e = \frac{1}{R} \frac{\text{length}}{\text{area}}$$

- Thus the bulk resistance of something depends on its size.
- Consider a sample of area A
 - The current I is constant
 - The voltage difference over a distance Δz (in the direction of the current flow) is $V_2 - V_1$.
 - Therefore the resistance is:

$$R = \frac{E}{I} = \frac{V_2 - V_1}{I}$$

- The flux of electrons $J_{e,z}$ or the current density is:

$$J_{e,z} = \frac{I}{A} = \frac{\sigma_e |V_2 - V_1|}{\Delta z}$$

- Resistance R , resistivity ρ_e , and conductivity σ_e , are all related by:

$$R = \frac{\Delta z}{\sigma_e A} = \frac{\rho_e \Delta z}{A}$$

- Electrical conductivities (S m^{-1}) span over 24 orders of magnitude for ordinary substances (not superconductors).
- Metals have high values:
 - Ag $6.3 \times 10^7 \text{ S m}^{-1}$
 - Cu $5.85 \times 10^7 \text{ S m}^{-1}$
 - Stainless steel $0.14 \times 10^7 \text{ S m}^{-1}$
- Conductivity of carbon depends on the form:
 - Graphite 10^5 S m^{-1}
 - Diamond 10^{-8} S m^{-1}
- Semiconductors span several orders of magnitude:
 - Si $2.52 \times 10^{-4} \text{ S m}^{-1}$
 - Ge 1.45 S m^{-1}
 - “gray” Sn 136 S m^{-1}

- Other elements
 - Iodine $7.7 \times 10^{-8} \text{ S m}^{-1}$
 - Sulphur $5 \times 10^{-16} \text{ S m}^{-1}$
- Polymers are often poor conductors:
 - Polyethylene $10^{-15} \text{ S m}^{-1}$
 - Polytetrafluoroethylene $10^{-17} \text{ S m}^{-1}$
- Conductivities of solutions depend strongly on the composition (i.e. electrolytes) of the solution.
- Conductivities of gases are extremely low unless the gas is subject to a high electric field that can ionize atoms and molecules.
- Conductivity and resistivity are temperature dependent.

Viscosity

- There are various types of viscosity. We will focus on shear viscosity.
- Viscosity is related to the flux of momentum.

- Newton's viscous law is:

$$J_{mv,zx} = -\eta \left(\frac{\partial v_x}{\partial z} \right)$$

- Flux, $J_{mv,zx}$, has units of momentum per unit time per unit area.
- However flux is easily interpreted as pressure because although momentum per unit time is a force, the direction of the force is parallel to the area and not perpendicular to it.
- Viscosity, η , has units of Pa s or poise (1 P = 0.1 Pa s)
- Hydrodynamics treats viscosity in great detail.
- Consider shear viscosity (Figure 25.9).
 - Consider an xz plane in a fluid.
 - Move a large thin plate (xy plane) in the x direction with velocity v_x .
 - A thin layer of fluid in contact with the plate moves with velocity v_x .

- The layer of fluid in contact with the fixed container is moving with zero velocity.
- This produces a velocity gradient in the z direction.
- If the container is not fixed and the fluid sufficiently viscous, then the motion of the plate will cause the container to move.
- This means that x momentum has been transferred along the z direction.
- This is an example of a shear force.
- This type of viscosity is called shear viscosity.

Some Representative Viscosities

- Cold molasses $\approx 1 \text{ Pa s}$
- Glycerol $\approx 1.5 \text{ Pa s}$
- Water $\approx 10^{-3} \text{ Pa s}$
- Viscosity may also be expressed in units of poise (P).
 - $1 \text{ Pa s} = 1 \text{ kg m}^{-1} \text{ s}^{-1}$
 - $1 \text{ P} = 1 \text{ g cm}^{-1} \text{ s}^{-1}$, therefore $1 \text{ P} = .1 \text{ Pa s}$;
 $1 \text{ cP} = 10^{-3} \text{ Pa s}$; $1 \mu \text{ P} = 10^{-7} \text{ Pa s}$.

Measuring Viscosity

- The Ostwald viscosimeter is a convenient instrument for measuring the viscosity of a liquid.
- Includes a vertical capillary tube.
 - The flow of a fluid through a tube is subject to a radial velocity gradient and flows fastest in the center.
 - Flow through a capillary is subject to laminar (non-turbulent) flow.
 - The viscous force is a friction.
 - If this friction is balanced by a hydrostatic head providing pressure, then steady-state flow results.
- The viscosity of the incompressible fluid is η .
- The tube is of length L and radius R .
- ΔP is the pressure difference between the top and bottom of the tube.
- r is the distance from the center of the tube.
 - The force pushing the fluid at r is $\Delta P \pi r^2$
- The contact area is $2\pi Lr$.

- The force per unit contact area is given by $(\Delta P \pi r^2)/(2\pi r L) = (\Delta P r)/(2L)$
- This force is exactly balanced by radial flux of z momentum. Therefore:

$$J_{mv,rz} = -\frac{\Delta P r}{2L} = -\eta \frac{\partial v_z}{\partial r}$$

- Thus the velocity v may be found as a function of r :

$$\begin{aligned} v_z(r) &= \int_{v_z(R)}^{v_z(r)} dv_z = -\frac{\Delta P}{2L\eta} \int_R^r r dr \\ &= \frac{\Delta P}{4L\eta} (r^2 - R^2) \end{aligned}$$

- The flow rate per unit time for an incompressible fluid becomes:

$$\frac{dV}{dt} = \frac{\Delta P \pi R^4}{8L\eta}$$

- The flow rate per unit time for a compressible fluid becomes:

$$\frac{dV}{dt} = \frac{\pi R^4}{16L\eta} \frac{P_i^2 - P_f^2}{P_0}$$

where

- P_i is the pressure at the tube's inlet,
 - P_f is the pressure at the tube's outlet,
 - P_0 is the pressure at which the volume is measured.
- The Ostwald viscometer is designed to exploit these equations.
 - Fill viscometer bulb with fluid of interest.
 - Draw fluid through capillary into calibrated bulb of volume V to above start mark.
 - Measure the time between the start and finish mark.
 - Calculate viscosity from:

$$\eta = \left(\frac{\pi R^4}{8L} \right) \frac{\rho g \langle \Delta h \rangle}{V} \Delta t$$

where ρ is the density of the fluid, g is gravitational acceleration, and $\langle \Delta h \rangle$ is the time average height difference:

$$\langle \Delta h \rangle = \frac{\Delta h_{start} - \Delta h_{finish}}{\ln(\Delta h_{start} / \Delta h_{finish})}$$

Microscopic Transport Coefficients

- Recall the linearized Boltzmann transport equation.
 - The solution gives the non-equilibrium number density distribution function, F^* .
 - Of more interest are the transport coefficients.
- Consider flux:

$$\text{flux} = \int \left(\begin{array}{c} \text{quantity} \\ \text{transported} \\ \text{per} \\ \text{molecule} \end{array} \right) \left(\begin{array}{c} \text{molecular} \\ \text{speed in} \\ \text{transport} \\ \text{direction} \end{array} \right) F^*(\mathbf{v}, \mathbf{r}, t) dv_x dv_y dv_z$$

- Applied to diffusion this becomes:

$$J_{n,z} = \int v_z F^*(\mathbf{v}, \mathbf{r}, t) dv_x dv_y dv_z = -D \left(\frac{\partial n}{\partial z} \right)$$

- Applied to thermal conductivity this becomes:

$$J_{q,z} = \int \frac{mv^2}{2} v_z F^*(\mathbf{v}, \mathbf{r}, t) dv_x dv_y dv_z = -k \left(\frac{\partial T}{\partial z} \right)$$

- Applied to electrical conductivity this becomes:

$$J_{e,z} = \int Qv_z F^*(\mathbf{v}, \mathbf{r}, t) dv_x dv_y dv_z = -\sigma_e \left(\frac{\partial \phi}{\partial z} \right)$$

- Applied to viscous flux of x momentum, this becomes:

$$\begin{aligned} J_{mv,zx} &= \int mv_x v_z F^*(\mathbf{v}, \mathbf{r}, t) dv_x dv_y dv_z \\ &= -\eta \left(\frac{\partial v_x}{\partial z} \right) \end{aligned}$$

- From each of these it is possible to derive the transport coefficient, since each flux expression imposes constraints on the Boltzmann transport equation.

The Diffusion Coefficient

- Assumptions:
 - Steady state, thus

$$\frac{\partial F^*}{\partial t} = 0$$

- No external forces, thus

$$\nabla_v F^* \cdot \frac{\mathbf{F}_{\text{ext}}}{m} = 0$$

- The concentration gradient is only in the z direction, thus:

$$\nabla F^* \cdot \mathbf{v} = \left(\frac{\partial F^*}{\partial z} \right) v_z$$

- Under these conditions, the Boltzmann equation becomes:

$$\frac{\partial F^*}{\partial z} v_z = - \frac{F^* - F}{\tau_{coll}}$$

- Further assume that F^* is close to F . Define the difference F' :

$$F^*(\mathbf{r}) = F(\mathbf{r}) + F'(\mathbf{r})$$

- Also assume that the spatial derivative of F' is negligible.

$$\left(\frac{\partial F^*}{\partial z} \right) \cong \left(\frac{\partial F}{\partial z} \right)$$

- With these further assumptions, the Boltzmann equation becomes:

$$\frac{\partial F}{\partial z} v_z = - \frac{F'}{\tau_{coll}}$$

- Isolating F' gives:

$$\begin{aligned} F' &= -\tau_{coll} \frac{\partial F}{\partial z} v_z = -\tau_{coll} v_z \frac{\partial F}{\partial n} \frac{\partial n}{\partial z} \\ &= \frac{-\tau_{coll} v_z F}{n} \frac{\partial n}{\partial z} \end{aligned}$$

- Substituting $F + F'$ for F^* gives:

$$\begin{aligned} J_{n,z} &= \int v_z F(\mathbf{v}, \mathbf{r}, t) dv_x dv_y dv_z \\ &\quad + \int v_z F'(\mathbf{v}, \mathbf{r}, t) dv_x dv_y dv_z \\ &= 0 + - \left(\frac{\tau_{coll}}{n} \int v_z^2 F d\mathbf{v} \right) \left(\frac{\partial n}{\partial z} \right) \end{aligned}$$

- Therefore:

$$D = \frac{\tau_{coll}}{n} \int v_z^2 F d\mathbf{v} = \frac{\tau_{coll}}{n} \left(\frac{nk_B T}{m} \right) = \frac{\tau_{coll} k_B T}{m}$$

since $F = nf$ and $\langle v_z^2 \rangle = k_B T/m$.

- Recalling that $\tau_{coll} = \lambda/\langle v \rangle$:

$$D = \frac{\lambda k_B T}{m \langle v \rangle} = \frac{1}{4n\sigma} \left(\frac{\pi k_B T}{m} \right)^{1/2}$$

$$= \left(\frac{\pi}{m} \right)^{1/2} \frac{(k_b T)^{3/2}}{4P\sigma}$$

where σ is the collision cross section and P is the pressure.

- Therefore:
 - Molecules with larger σ diffuse more slowly than ones with smaller σ .
 - Diffusion slows as P increases
 - Diffusion is faster at higher T

Thermal Conductivity

- A temperature gradient at constant pressure means that there is a density gradient.

$$P = nk_B T$$

where n is the density N/V

- If $\partial T / \partial z \neq 0$ then $\partial n / \partial z \neq 0$ to maintain constant P .

- This means that the local equilibrium distribution function explicitly depends on z through $n(z)$ and $T(z)$:

$$F(z) = n(z) \left(\frac{m}{2\pi k_B T(z)} \right)^{\frac{3}{2}} e^{-m(v_x^2 + v_y^2 + v_z^2)/2k_B T(z)}$$

- Following the same procedure as we used for diffusion, the Boltzmann transport equation becomes:

$$F' = -v_z \tau_{coll} \left(\frac{\partial F(z)}{\partial z} \right)$$

and

$$\frac{\partial F(z)}{\partial z} = \frac{F}{T} \left(\frac{mv^2}{2k_B T} - \frac{5}{2} \right) \left(\frac{\partial T}{\partial z} \right)$$

- Thus $J_{q,z}$ becomes:

$$\begin{aligned} J_{q,z} &= \int \left(\frac{mv^2}{2} \right) v_z F' d\mathbf{v} \\ &= - \left[\frac{\tau_{coll}}{T} \int \left(\frac{mv^2}{2} \right) v_z^2 \left(\frac{mv^2}{2k_B T} - \frac{5}{2} \right) F d\mathbf{v} \right] \left(\frac{\partial T}{\partial z} \right) \end{aligned}$$

- Integration yields:

$$k = \frac{5}{2} \frac{\tau_{coll} n k_B^2 T}{m}$$

- Using $\overline{C}_v = 3N_A k_B/2$ for an ideal monatomic gas, this becomes:

$$k = \frac{5}{2} \frac{\lambda n k_B^2 T}{m \langle v \rangle} = \frac{5}{2} \frac{k_B^{3/2}}{4\sigma} \left(\frac{\pi T}{m} \right)^{1/2}$$

$$= \frac{5}{12} \frac{\overline{C}_V}{\sigma N_A} \left(\frac{\pi k_B T}{m} \right)^{1/2}$$

- Thus thermal conductivity k
 - decreases for heavier molecules
 - increases with temperature
 - is independent of pressure, but the expression breaks down at low pressures and extremely high pressures.
- At intermediate pressures, the P dependence of λ is cancelled out by the P dependence of n .
- If the pressure is so low that λ is greater than the thickness of the gas layer through which the heat is conducted, then k becomes P dependent and the heat transfer does not depend on collisions.
- At high pressures, multiple collisions become an important means of heat transfer.

Electrical Conductivity

- Consider a weakly ionized gas (i.e. a plasma)
 - n_+ is the number density of positively charged ions, each with a charge of Q_+ .
 - Sufficient electrons or anions are present to balance the charge and assure that the plasma is electrically neutral.
- While the net current is due to motion of all charged species, the movement of positive charges will be initially considered.
- Impose on a plasma a small potential gradient,

$$\frac{\partial \phi}{\partial z} = -E_z$$

due to the z component of the external electric field.

- Thus the flux gradient equation becomes:

$$J_{e,z} = \sigma_e E_z$$

- Assume that ions and neutrals have the same f^* .

- This is reasonable because of collisions.
- Assume that $n_+ \ll n$
 - For the positive ions, $F^* = n_+ f^*$.
 - For the neutrals $F^* = n f^*$.
- Assume that the deviation, F' from equilibrium is small.

$$F^* = F + F'$$

- The Boltzmann equation has no spatial gradient term ($\nabla F^* = 0$), but is subject to an external force ($F_{ext,z} = Q_+ E_z$).
- Thus:

$$\nabla F^* \cdot \mathbf{v} + \nabla_v F^* \cdot \frac{\mathbf{F}_{ext}}{m} + \frac{\partial F^*}{\partial t} = -\frac{F^* - F}{\tau_{coll}}$$

becomes:

$$\frac{\partial F}{\partial v_z} \frac{Q_+ E_z}{m} = -\frac{F'}{\tau_{coll}}$$

which rearranges to:

$$F' = -\frac{\tau_{coll} Q_+ E_z}{m} \frac{\partial F}{\partial v_z}$$

- Since F is the equilibrium distribution,

$$\frac{\partial F}{\partial v_z} = -\frac{mv_z}{k_B T} F$$

$$F' = \frac{\tau_{coll} Q_+ E_z}{k_B T} v_z F$$

- Because $F' \ll F$, the electric field, E_z is small.
- The expression for flux becomes:

$$J_{e,z} = Q_+ \int v_z F' d\mathbf{v} = \left(\frac{\tau_{coll} Q_+^2}{k_B T} \int v_z^2 F d\mathbf{v} \right) E_z$$

where

$$\sigma_e = \frac{\tau_{coll} Q_+^2}{k_B T} \int v_z^2 F d\mathbf{v} = \frac{n_+ \tau_{coll} Q_+^2}{m}$$

- If it is assumed that the ions have the same cross section as the neutrals, then a substitution may be made for τ_{coll} :

$$\sigma_e = \frac{\lambda n_+ Q_+^2}{m \langle v \rangle} = \frac{n_+}{n} \frac{Q_+^2}{4\sigma} \left(\frac{\pi}{mk_B T} \right)^{1/2}$$

- Note that the charge term is squared so that σ_e is always positive.

- It is necessary to consider other ions and other charges that are present in the solution.
 - The concept of ion mobility u is useful.
 - u is the ions' drift velocity per unit electrical field or conductivity per unit of charge concentration.

$$\begin{aligned}
 u_+ &= \frac{\text{conductivity}}{\text{unit charge concentration}} = \frac{\sigma_e}{n_+ Q_+} \\
 &= \frac{\tau_{coll} Q_+}{m} = \frac{Q_+}{4n\sigma} \left(\frac{\pi}{mk_B T} \right)^{1/2}
 \end{aligned}$$

- For two species of opposite charge with ion mobilities of u_+ and u_- , the net conductivity is:

$$\sigma_e = \sigma_+ + \sigma_- = n_+ Q_+ u_+ + n_- Q_- u_-$$

- The ratio of mobility to the diffusion coefficient is:

$$\frac{u_+}{D} = \frac{\tau_{coll} Q_+}{m} \frac{m}{\tau_{coll} k_B T} = \frac{Q_+}{k_B T}$$

Viscosity

- Consider a gas with a slow *bulk flow* in the x direction and a flow gradient in the z direction.
- The flow speed is u_x is additive to the velocity vectors of the molecule, yielding local velocity components (U_x, U_y, U_z) with respect to the *flowing* frame of reference:

$$U_z = v_z, \quad U_y = v_y, \quad U_x = v_x - u_x$$

- Assume
 - A steady state flow
 - That the distribution is slightly perturbed from equilibrium such that:

$$F^* = F + F'$$

- Thus, it can be shown that:

$$\begin{aligned} F' &= -\tau_{coll} v_Z \frac{\partial F}{\partial z} = -\tau_{coll} v_Z \left(\frac{\partial F}{\partial U_x} \right) \left(\frac{\partial U_x}{\partial z} \right) \\ &= -\tau_{coll} v_Z \left(\frac{\partial F}{\partial u_x} \right) \left(\frac{\partial u_x}{\partial z} \right) \end{aligned}$$

- The flux expression becomes:

$$\begin{aligned}
 J_{mx,zx} &= \int (mU_x)U_z F' d\mathbf{U} = m \int U_x v_z F' d\mathbf{U} \\
 &= \left[\tau_{coll} m \int \left(\frac{\partial F}{\partial U_x} \right) U_x v_z^2 d\mathbf{U} \right] \left(\frac{\partial u_x}{\partial z} \right)
 \end{aligned}$$

- Thus:

$$\begin{aligned}
 \eta &= -\tau_{coll} m \int \left(\frac{\partial F}{\partial U_x} \right) U_x v_z^2 d\mathbf{U} \\
 &= -\tau_{coll} m \int \left(-F \frac{mU_x}{k_B T} \right) U_x v_z^2 d\mathbf{U} \\
 &= \frac{\tau_{coll} m^2}{k_B T} \int F U_x^2 v_z^2 d\mathbf{U} = \frac{\tau_{coll} m^2}{k_B T} n \left(\frac{k_B T}{m} \right)^2 \\
 &= n \tau_{coll} k_B T
 \end{aligned}$$

- And substituting for τ_{coll} yields:

$$\eta = \frac{n \lambda k_B T}{\langle v \rangle} = \frac{(\pi k_B T m)^{1/2}}{4\sigma}$$

- Thus for a gas:

- η increases with temperature.
- η is independent of pressure.